

Amendments to the Specification:

**Please replace paragraph [0019] beginning at page 10, line 5 with the following amended paragraph:**

--Thus, as shown in Fig. 3(d), even when a high-level clock signal is outputted from the oscillator 6 at intervals of a time period  $t_b$ , the RS flip-flop 5 continues to output a low-level signal, as shown in Fig. 3(c), because a high-level signal is inputted from the comparator 4 to the reset terminal of the RS flip-flop 5, as shown in Fig. 3(e). Thus, the driver 1 keeps the MOS transistor Tr1 off and the MOS transistor Tr2 on.--

**Please replace paragraph [0021] beginning at page 11, line 1 with the following amended paragraph:**

-- Thus, the driver 1 turns the MOS transistor Tr1 on and the MOS transistor Tr2 off, whereby a current begins to flow through the coil L, as shown in Fig. 3(a). As a result, the voltage VL inputted to the inverting input terminal of the comparator 4 is dropped by the current IL flowing through the coil L. As the current IL flowing through the coil L increases, as shown in Fig. 3(a), the voltage VL inputted to the inverting input terminal of the comparator 4 decreases, as shown in Fig. 3(b). When the voltage VL becomes lower than the voltage  $V_{th}$  from the level shifter 3, as shown in Fig. 3(b), the signal from the comparator 4 is switched to high level, as shown in Fig. 3(e). As a result, the signal from the RS flip-flop 5 turns to low level, as shown in Fig. 3(c).--

**Please replace paragraph [0027] beginning at page 13, line 11 with the following amended paragraph:**

--Furthermore, as shown in Fig. 4, a resistance Ra is connected, at one end thereof, to the inverting input terminal of the comparator 4 and, at the other end thereof, to a node at which the source of the MOS transistor Tra and the drain of the MOS transistor Trb are connected together, and a constant-current power supply I1 that feeds a constant current is connected to the inverting

input terminal of the comparator 4. The other end of the constant-current power supply 11 is grounded. In this way, by connecting the resistance  $R_a$  and the constant-current power supply 11 together, a voltage drop  $R_a \times I_{off}$  across the resistance  $R_a$  caused by the passage of a constant current  $I_{off}$  fed from the constant-current power supply 11 through the resistance  $R_a$  is added as an offset voltage  $V_{off}$ . That is, the resistance  $R_a$  and the constant-current power supply ~~10~~ 11 function as a voltage source 20.--

**Please replace paragraph [0035] beginning at page 16, line 4 with the following amended paragraph:**

--As is the case of the first embodiment, also in this embodiment, when a heavy load is connected as described above, the voltage obtained by detecting the current  $I_L$  flowing through the coil  $L$  is sufficiently higher than the offset voltage  $V_{xoff}$  from the voltage source 20a. That is, the voltage values  $V_{hoff}$  and  $V_{loff}$  added as an offset voltage  $V_{xoff}$  each fall within the voltage range in which the influence thereof on the voltage  $V_L$  inputted to the inverting input terminal of the comparator 4 is so small that it can be ignored.--

**Please replace paragraph [0042] beginning at page 19, line 8 with the following amended paragraph:**

--When a current detection circuit 10 having the same configuration as that shown in Fig. 4 of the first embodiment is incorporated in the switching power supply apparatus described above, the relation of connection between the current detection circuit 10 and the comparator 4 is shown in Fig. 8. In this case, as shown in Fig. 8, a resistance  $R_a$  used for adding an offset voltage  $V_{off}$  is replaced with a variable resistance  $R_b$  that can switch a resistance value depending on the output of the comparator 4. That is, the variable resistance  $R_b$  and the constant-current power supply 11 constitute a voltage source ~~21a~~ 20a. Other circuit blocks are the same as those in Fig. 4.--

**Please replace paragraph [0053] beginning at page 23, line 3 with the following amended paragraph:**

--When the slope compensation voltage  $V_{slope}$  from the voltage source 21 decreases from a maximum value  $V_{Smax}$  to a minimum value of zero, as shown in Fig. 11(f), immediately before a clock is outputted from the oscillator 5 6, as shown in Fig. 11(c), the voltage  $V_{th}$  outputted from the level shifter 3 becomes lower than the voltage  $V_L$ , as shown in Fig. 11(b). That is, when the value of the voltage  $V_L$  fed to the inverting input terminal of the comparator 4 increases by changing from  $V_{cc} - V_{off} - V_{Smax}$  to  $V_{cc} - V_{off}$ , as shown in Fig. 11(b), the voltage  $V_{th}$  becomes lower than the voltage value given by  $V_{cc} - V_{off}$ --

**Please replace paragraph [0054] beginning at page 23, line 4 with the following amended paragraph:**

--At this time, as shown in Fig. 11(e), a low-level signal is outputted from the comparator 4, and, immediately after the slope compensation voltage  $V_{slope}$  decreases from a maximum value  $V_{Smax}$  to a minimum value of zero, a high-level clock signal is outputted from the oscillator 6, as shown in Fig. 7(d) 11(d). Thus, a high-level signal is inputted to the set terminal of the RS flip-flop 5 after a low-level signal is inputted to the reset terminal thereof, whereby the signal from the RS flip-flop 5 is switched to high level, as shown in Fig. 11(c). On the other hand, after the slope compensation voltage  $V_{slope}$  reaches to a minimum value of zero, it gradually increases again, as shown in Fig. 11(f). Thus, as shown in Fig. 11(b), as the slope compensation voltage  $V_{slope}$  increases, the voltage  $V_L$  fed to the inverting input terminal of the comparator 4 decreases.--

**Please replace paragraph [0057] beginning at page 25, line 12 with the following amended paragraph:**

--When a current detection circuit 10 having the same configuration as that shown in Fig. 4 of the first embodiment is incorporated in the switching power supply apparatus described above, the relation of connection between the current detection circuit 10 and the comparator 4 is

shown in Fig. 12. In this case, as shown in Fig. 12, the current source 21 is built with an n-channel MOS transistor Trx that is connected, at the drain thereof, to a node at which the resistance Ra and the constant-current power supply 11 are connected together, a MOS transistor Try that is connected, at the gate and the drain thereof, to the gate of the MOS transistor Trx, a MOS transistor Trz that is connected, at the drain thereof, to the source of the MOS transistor Try, a resistance Rc that is connected to the source of the MOS transistor Trx, a capacitor C1 that is connected to the source of the MOS transistor Try, and a constant-current power supply 12 that is connected to the drain of the MOS transistor ~~Try~~ Try. Other circuit blocks are the same as those in Fig. 4.--

**Please replace the heading at the top of page 30 with the following:**

--

**CLAIMS**

**What is claimed is: --**